## Sorption of carbon dioxide by the composite sorbent "potassium carbonate in porous matrix"

A. G. Okunev, \* V. E. Sharonov, A. V. Gubar', I. G. Danilova, E. A. Paukshtis, E. M. Moroz, T. A. Kriger, V. V. Malakhov, and Yu. I. Aristov

G. K. Boreskov Institute of Catalysis, Siberian Branch of the Russian Academy of Sciences, 5 prosp. Akad. Lavrent eva, 630090 Novosibirsk, Russian Federation.

Fax: +7 (383 2) 34 3056. E-mail: okunev@catalysis.nsk.su

Sorption of  $CO_2$  in the presence of water vapor by the  $K_2CO_3$ — $\gamma$ - $Al_2O_3$  composite sorbent was studied by IR spectroscopy *in situ*, X-ray diffraction analysis, and the differentiating dissolution method and reasons for a decrease in its dynamic capacity are given. The samples containing  $K_2CO_3 \cdot 1.5H_2O$  in pores are characterized by the maximal dynamic capacity. A mechanism for  $CO_2$  sorption was proposed, which qualitatively explains the obtained dependence of the capacity on the water content in the composite sorbent. A high dynamic capacity can be maintained by regeneration of the sorbents by water vapor at 170 °C. The capacity of the sorbents decreases during the first 10 sorption—regeneration cycles due to the formation of an inactive phase of potassium aluminum carbonate.

**Key words:** composite sorbent, chemisorption, carbon dioxide, potassium carbonate, IR spectroscopy *in situ*.

The problem of CO<sub>2</sub> sorption by solid sorbents at ~100 °C under conditions of a high moisture content in the gas mixture is of basic significance for the creation of adsorption systems for CO<sub>2</sub> removal from flue gases. The capacity of conventional microporous sorbents based on the zeolites or activated carbons toward CO<sub>2</sub> decreases in a wet atmosphere and at temperatures higher than 40 °C, which makes their use inefficient. One of the most promising sorbents for CO2 extraction from flue gases is the potassium carbonate-porous matrix system, proposed earlier by several groups of researchers.<sup>2-6</sup> In particular, the potassium carbonate—porous carbon sorbent, whose dynamic capacity before the onset of the breakthrough in a flow-type absorber is  $\sim 30$  mg  $CO_2$   $g^{-1}$  of sorbent, has been described.<sup>3,7,8</sup> The sorption of CO<sub>2</sub> results in the transformation of potassium carbonate into hydrocarbonate

$$K_2CO_3 + CO_2 + H_2O \rightleftharpoons 2 KHCO_3$$

and at temperatures higher than 150 °C the equilibrium shifts substantially toward reactants. This sorbent possesses a high dynamic capacity only when the salt introduced into the matrix pores exists in the form of hydrate  $K_2 \text{CO}_3 \cdot 1.5 \text{H}_2 \text{O}$ . To achieve such a phase composition, the composite is regenerated before sorption by steam at  $150 \, ^{\circ}\text{C}.^3$ 

It is difficult to use this sorbent in practice because of its low dynamic capacity. In fact, the high porosity of activated carbons ( $\sim$ 0.4 g cm<sup>-3</sup>) results in the situation that the dynamic capacity per sorbent volume unit is only 11-13 mg cm<sup>-3</sup>. Such a composite material can be used only in very large adsorbers.

It has previously been shown<sup>9,10</sup> that in another composite system, viz.,  $K_2CO_3$ — $\gamma$ - $Al_2O_3$ , the dynamic capacity toward  $CO_2$  as high as 90 mg g<sup>-1</sup> can be reached, although this index decreases considerably already after the first regeneration.<sup>11,12</sup> The present work is an attempt to study the mechanism of  $CO_2$  sorption by the  $K_2CO_3$ — $\gamma$ - $Al_2O_3$  system and to reveal reasons for decreasing dynamic capacity of these sorbents.

## **Experimental**

The supporting matrix was  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> produced at the ONPZ plant (Omsk, Russia) with a pore volume of 0.7 g cm<sup>-3</sup> and a specific surface area of 220 m² g<sup>-1</sup>. The support was impregnated with a 40% aqueous solution of K<sub>2</sub>CO<sub>3</sub>. The solvent was removed by drying in a desiccator at 200 °C or on a rotary evaporator using a boiling water bath. The salt content in the completely dried sample was 26.8 wt.%. The elution sorption curves were obtained at 40 °C, passing a mixture of wet air (with the relative moisture content about 90% at ~20 °C) and CO<sub>2</sub> (CO<sub>2</sub> content 2 vol.%) through a flow-type cylindrical adsorber at a flow rate of 150 mL min<sup>-1</sup>. The sorbent (4 g, ~5 mL, fraction 0.5–1.0 mm) was placed in an adsorber 6 mm in diameter and 180 mm in length. The content of CO<sub>2</sub> at the outlet was measured using an IR detector with a relative accuracy of ~2% in the 200–20000 ppm region. The dynamic capacity  $A_{\rm dyn}$  was

calculated as a ratio of the amount of  $CO_2$  sorbed by the sorbent before the onset of the breakthrough (i.e., before the sharp increase in the  $CO_2$  content at the adsorber outlet) to the sorbent weight. The temperature plot of the dynamic capacity in the  $20-80\,^{\circ}\mathrm{C}$  region was measured by maintaining a constant temperature of the adsorbent using a water thermostat, and at higher temperatures the adsorber was placed in a furnace with automated temperature monitoring.

IR spectra were recorded on a FTIR-8300 spectrometer (Shimadzu) in the 700–6000 cm $^{-1}$  with a resolution of 4 cm $^{-1}$ . Before recording spectra, samples were pressed to give pellets with  $\rho=20-30~\text{mg}~\text{cm}^{-2}$ , using CaF $_2$  as diluent, with the sample content 10–20%. Gas sorption was studied in a flow-type steel cell with CaF $_2$  windows. This design of the cell makes it possible to heat pellets to 250 °C. A mixture containing 2% CO $_2$  and 98%  $N_2$  was saturated with water vapor on passing through a bubbler flask and introduced to a sample with a rate of  $\sim\!\!30~\text{mL}~\text{min}^{-1}$ .

A Freiberg HZG-4 X-ray diffractometer with  $CuK\alpha$  radiation and a graphite monochromator was used for detection *ex situ* of powder diffraction patterns.

Diffraction experiments *in situ* were carried out on a Siemens D-500 X-ray diffractometer using CuK $\alpha$  radiation and a graphite monochromator on a diffraction beam. Measurements at elevated temperatures were carried out in a special X-ray chamber. A sample was placed in the chamber and heated in a He flow to 50 °C. After this temperature was achieved, a gas mixture containing 2% CO<sub>2</sub>, 2% H<sub>2</sub>O, and 96% He was loaded in the chamber, and after 30 min a diffraction pattern was detected. Then the sample was heated to a required temperature and stored for 30 min, and the diffraction pattern of the sample was measured again. Then the sample was cooled in a pure He flow to 50 °C, and CO<sub>2</sub> sorption was carried out. The heating velocity did not exceed 5 K min<sup>-1</sup>. Diffraction patterns were detected in the  $10^{\circ}-75^{\circ}$  (20) region by points with the  $0.05^{\circ}$  (20) step.

Differentiating dissolution was performed in the flow-type regime, passing water, a solution of HCl with pH 2, and 25%  $H_2 SO_4$  through the sample to its complete dissolution. The content of potassium and aluminum in the resulting solution was continuously measured using an atomic emission spectrometer with inductively coupled plasma to obtain kinetic curves of dissolution. Time intervals, during which a constant molar ratio of concentrations of the  $Al^{3+}$  to  $K^+$  cations in the dissolution products is observed, correspond to the dissolved state of individual phases.  $^{14}$ 

## **Results and Discussion**

It is found that conditions of synthesis have a decisive effect on the dynamic capacity of freshly prepared sorbents. For example,  $A_{\rm dyn}$  of the sorbent prepared by calcination in air at 200 °C is several times lower than that of the sample dried on a rotary evaporator (Fig. 1). The influence of drying is mainly determined by the amount of water remaining in the sorbent after drying (Fig. 2). The maximum of dynamic activity corresponds to the formation of  $K_2CO_3 \cdot 1.5H_2O$  in the matrix pores.

The influence of crystallization water on CO<sub>2</sub> adsorption was studied by IR spectroscopy *in situ* to reveal rea-

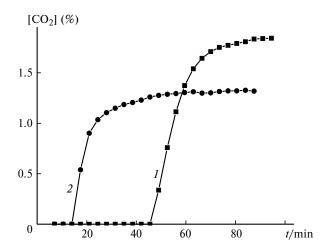


Fig. 1. Plot of the  $CO_2$  concentration at the adsorber outlet vs. time for the sorbent dried on a rotary evaporator at  $100 \,^{\circ}\text{C}$  (I) and calcined at  $200 \,^{\circ}\text{C}$  in a desiccator (2). Temperature of sorption  $40 \,^{\circ}\text{C}$ .

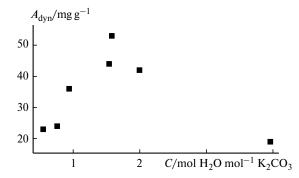


Fig. 2. Dynamic capacity of the freshly prepared samples dried on a rotary evaporator vs. residual water content (C). Temperature of sorption 40 °C.

sons for a high dynamic capacity observed in the presence of  $K_2CO_3 \cdot 1.5H_2O$  impregnated into a porous matrix. Three samples were used for the studies: sample 1 represented supported crystal hydrate  $K_2CO_3 \cdot 1.5H_2O/Al_2O_3$ , sample 2 was prepared by heating sample 1 at 200 °C in the reaction mixture for 30 min, and sample 3 was prepared by storing sample 2 for 30 min in an  $N_2$  flow saturated by water vapor. In the IR spectra of samples 1-3 (Fig. 3), the intensity of the absorption band at  $3200 \text{ cm}^{-1}$ , which characterizes  $v_{OH}$  of crystallization water, decreases in the series 1 > 3 > 2. In addition, an absorption band at  $3445 \text{ cm}^{-1}$ , which is characteristic of  $KAl(CO_3)_2$ , appears in the IR spectra of samples 2 and 3 (see Fig. 3).

The study of  $CO_2$  sorption on samples 1—3 revealed the formation of intermediate compounds of the same type, viz.,  $HCO_3^-$  anion (1270 cm<sup>-1</sup>) and dehydrated  $K_2CO_3$  (1315 cm<sup>-1</sup>) (Fig. 4). According to the data obtained, a decrease in the amount of crystallization water in the series of samples 1 > 3 > 2 decreases the maximal concentration of intermediate compounds formed upon

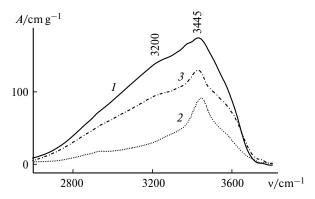
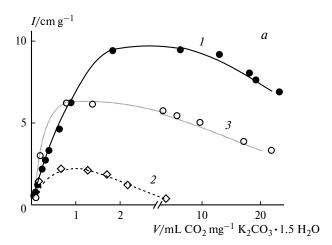
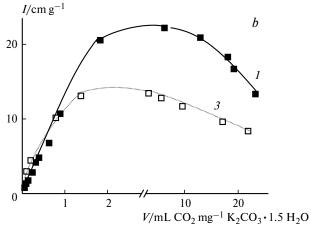


Fig. 3. IR spectra of samples 1-3 (curves I-3) in the region of absorption of OH groups (for conditions of preparation of the sample, see text). The integral absorption per 1 g of the sample is put on the ordinate.

CO<sub>2</sub> sorption (see Fig. 4). Thus, CO<sub>2</sub> sorption appears to be accompanied by the insertion of its molecule into the





**Fig. 4.** Change in the integral absorption I (*i.e.*, difference between the initial and current values of integral sorption per 1 g of sorbent) for absorption bands at 1315 (a) and 1270 cm<sup>-1</sup> (b) in the IR spectra of the samples obtained on introducing a  $2\% \text{ CO}_2 + 2\% \text{ H}_2\text{O} + 96\% \text{ N}_2$  mixture to sorbents 1-3 (curves I-3).

K<sub>2</sub>CO<sub>3</sub>·1.5H<sub>2</sub>O structure to form intermediate compounds, whose concentration increases first rapidly, reaches a maximum, and then decreases slowly due to their secondary transformations to form KHCO<sub>3</sub>. A possible mechanism of sorption can be presented by the following scheme:

$$\begin{split} \text{K}_2\text{CO}_3 \cdot 1.5\text{H}_2\text{O} + \text{CO}_2 & \xrightarrow{\text{rapidly}} \\ & \longrightarrow \text{HCO}_3^- + \text{H}^+ + \text{K}_2\text{CO}_3 + 0.5 \text{ H}_2\text{O}, \\ \\ \text{HCO}_3^- + \text{H}^+ + \text{K}_2\text{CO}_3 & \xrightarrow{\text{slowly}} \quad 2 \text{ KHCO}_3. \end{split}$$

In the absence of a sufficient amount of crystallization water, this scheme is supplemented by the step of addition of a water molecule from the gas phase

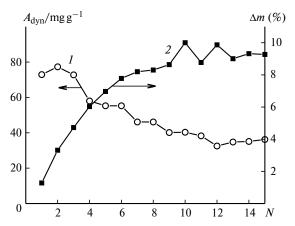
$$K_2CO_3 + x H_2O \xrightarrow{slowly} K_2CO_3 \cdot x H_2O$$

which, most likely, is the process-limiting step. The concentration of adsorbed  $\mathrm{CO}_2$  corresponding to a maximum of formation of intermediate compounds (see Fig. 4) correlates well with the dynamic capacity of the sorbent (cf. Fig. 1).

Thus, the IR spectroscopic results suggest that crystal-lization water bound to potassium carbonate has a decisive effect on  $CO_2$  sorption. It is most likely that this is the "pre-dissociation" <sup>15</sup> state of water in  $K_2CO_3 \cdot 1.5H_2O$  that favors the efficiency of the reaction with  $CO_2$  to form the  $HCO_3^-$  anion. When the water content is higher than 1.5  $H_2O$  molecules per  $K_2CO_3$  molecule, a solution with a low rate of  $CO_2$  sorption forms in the pores, and  $A_{\rm dyn}$  of the sorbent decreases (see Fig. 2). This agrees with a low rate of  $CO_2$  absorption by a solution of  $K_2CO_3$ . In this case, an increase in the reaction rate is achieved by the introduction of such promoters as secondary or tertiary amines into the solution or by the temperature rise. <sup>16</sup>

Correspondingly, the efficient regeneration of the sorbent after the sorption stage needs the formation of  $K_2CO_3 \cdot 1.5H_2O$  in pores. Sorbent regeneration by steam at 150-200 °C decomposes the most part of hydrocarbonate to form  $K_2CO_3 \cdot 1.5H_2O$ . This method for regeneration of the  $K_2CO_3 \cdot 1.5H_2O$ . This method for regeneration of the  $K_2CO_3-\gamma-AI_2O_3$  sorbent stabilizes the dynamic capacity, which after 10 sorption—regeneration cycles reaches a stationary level of 35 mg  $CO_2$  g<sup>-1</sup> of the sorbent (Fig. 5), ~40% of the initial activity of the sorbent. It turned out that a decrease in  $A_{\rm dyn}$  is accompanied by an increase in the weight of the dry sorbent (see Fig. 5), indicating a change in its chemical composition.

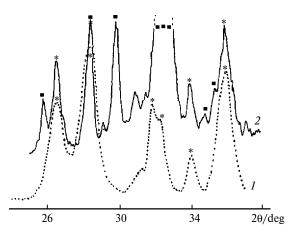
According to the X-ray diffraction data, the samples of the  $K_2CO_3$ — $\gamma$ - $Al_2O_3$  composite sorbent contains the  $KAl(CO_3)_2 \cdot 1.5H_2O$  phase, which appears at the stage of preparation when  $K_2CO_3$  introduced into the pores interacts with the  $Al_2O_3$  matrix (Fig. 6). The measurement in a



**Fig. 5.** Dynamic capacity of the sorbent (1) and the weight increment (2)  $\nu s$ . number of sorption—regeneration cycles (N). Sorption of  $CO_2$  from wet air was carried out at 40 °C, and regeneration was carried out by steam blowing (1 atm) at 170 °C.

flow-type adsorber of  $A_{\rm dyn}$  of pure KAl(CO<sub>3</sub>)<sub>2</sub>·1.5H<sub>2</sub>O prepared by a known procedure<sup>17</sup> showed that this aluminum carbonate did not manifest the sorption activity toward CO<sub>2</sub>. Therefore, upon the formation of the potassium aluminum carbonate phase a portion of K<sub>2</sub>CO<sub>3</sub>·1.5H<sub>2</sub>O is transformed i nto the inactive form, and  $A_{\rm dyn}$  of the sorbent decreases.

The phase distribution of potassium cations in the sorbent was studied by the differentiating dissolution method. The calculations showed that if the  $KAl(CO_3)_2 \cdot 1.5H_2O$  phase incorporated in the freshly prepared sorbent contains 13% of the total amount of potassium cations in the sorbent, then after 10 sorption—regeneration cycles more than 50%  $K^+$  cations are transferred to this phase. Further the amount of  $KAl(CO_3)_2 \cdot 1.5H_2O$  is most likely stabilized (see Fig. 5) due to a decrease in the free alumina surface accessible for



**Fig. 6.** Diffraction patterns of the KAl(CO<sub>3</sub>)<sub>2</sub>·1.5H<sub>2</sub>O phase (*I*) and  $K_2CO_3$ —Al<sub>2</sub>O<sub>3</sub> composite sorbent (*2*). Peaks of the KAl(CO<sub>3</sub>)<sub>2</sub>·1.5H<sub>2</sub>O phase are marked by asterisks, and those of  $K_2CO_3$ ·1.5H<sub>2</sub>O are marked by squares.

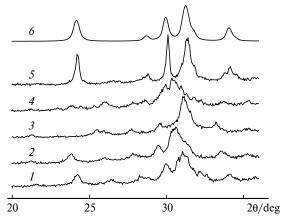
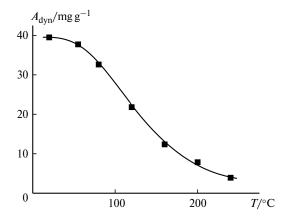


Fig. 7. Diffraction patterns of the composite sorbents (1-5) after sorption (1), after heating to 100 (2) and 200 °C (3), after secondary sorption (4), and after storage in air for 14 days (5) and diffraction pattern of pure KHCO<sub>3</sub> (6).



**Fig. 8.** Plot of the stationary dynamic capacity of the sorbent vs. temperature of sorption.

the reaction. The potassium aluminum carbonate phase is unstable upon prolonged storage of the samples in air and decomposes to form KHCO<sub>3</sub> (Fig. 7).

It is of great interest to measure  $A_{\rm dyn}$  at different temperatures for analysis of possible practical applications of the new sorbent. The dynamic capacity of the new materials decreases fairly slowly with the temperature rise, so that even at 120 °C it exceeds 20 mg g<sup>-1</sup> (Fig. 8). As the temperature increases to 200 °C,  $A_{\rm dyn}$  decreases to 7 mg g<sup>-1</sup>. Compared to the previously proposed potassium carbonate—activated carbon system,<sup>3</sup> the new sorbent has a substantially higher capacity per volume unit. Using a bulk density of the sorbent of 0.85 g cm<sup>-3</sup>, one can easily calculate the stationary capacity (~30 mg CO<sub>2</sub> cm<sup>-3</sup>), which is approximately 2.5-fold higher than that of the analogous system on porous carbon.

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